# The Analytical Representation of Atomic Scattering Amplitudes for Electrons

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A single analytical expression to represent the published values of the atomic scattering amplitudes for electrons  $f_e(x)$  is given, and the parameters are determined for elements Z = 1-18 and 20-104. Three terms are sufficient to fit the data accurately for all elements and all values of  $f_e(x)$  are

given equal weight. The standard deviation has an average value of 0.22% of  $f_e(0)$ .

### Introduction

In connection with the preparation of the third volume of the International Tables for Crystallography Ibers (1958), Vainshtein & Ibers (1958) and Ibers & Vainshtein (1959) have published values of the atomic scattering amplitudes for electrons  $f_e(x)$  for specific values of  $x = \sin \theta / \lambda$  and for elements with atomic numbers Z in the ranges 1-18 and 20-104. In view of the importance of  $f_e(x)$  both in electron diffraction, where Fourier methods are being used increasingly (e.g. Cowley & Rees, 1958), and in a study of the contrast arising by elastic electron scattering in electron microscopy (for references see Burge & Smith, 1961), it was considered desirable to express  $f_e(x)$  for each element by a single analytical expression from which values could be calculated for any value of x and any electron energy.

The data given by Ibers & Vainshtein cover the range of x from 0 to  $1.0 \text{ Å}^{-1}$  for the elements Z=1-18 and the range from 0 to  $1.5 \text{ Å}^{-1}$  for Z=20-104. The atomic model used in the calculation of  $f_{\ell}(x)$  is listed in Table 2 together with the corresponding analytic constants for the elements concerned.

A number of analytical expressions for f(x) have been published (Vand, Eiland & Pepinsky, 1957; Freeman & Smith, 1958; Forsyth & Wells, 1959; Silverman & Simonsen, 1960). The forms of the curves for f(x) and  $f_e(x)$  are sufficiently similar to justify the assumption that any of these analytical forms would also fit the data for  $f_e(x)$ .

# The analytical representation of $f_e(x)$

It was decided to use the expression

$$f_e(x) = \sum_j A_j \exp\left(-B_j x^2\right), \qquad (1)$$

since it was considered important that the terms should be of the same form with constant  $A_j$  and  $B_j$ for all values of x and that the terms should be easy to integrate over a range of x (for this application to the theory of elastic electron scattering at very small angles, see Burge & Smith, 1961). It was found that for all elements, only three terms in equation (1) were necessary to give a good fit.

# Criterion of goodness of fit

The difference between the data value of the atomic scattering amplitude  $f_e(x)$  and the analytical value e(x) for each point was expressed as a percentage of  $f_e(x)$  given by

$$G(x) = \left[\frac{e(x) - f_e(x)}{f_e(x)}\right] \times 100 .$$
<sup>(2)</sup>

The sum of the squares of the percentage errors was then given by

$$W = \sum_{i=1}^{M} [G_i(x)]^2, \qquad (3)$$

where M was the number of data points available, and W was minimized to give the best possible fit.

Equation (2) (Freeman & Smith, 1958) was regarded as a better criterion than expressing the difference between e(x) and  $f_e(x)$  as a percentage of  $f_e(0)$  (Vand *et al.*, 1957), since it ensures the same degree of fit along the whole length of the curve. When the best fit had been obtained the standard deviation of the analytical curve from the data was expressed as a percentage of  $f_e(0)$ , by the equation

$$Y = (100/f_e(0)M^{\frac{1}{2}}) \left\{ \sum_{i=1}^{M} [e(x_i) - f_e(x_i)]^2 \right\}^{\frac{1}{2}}.$$
 (4)

### Method of evaluating constants

(a) First approximation (two terms)

Initially two terms of equation (1) were considered. If the fit is perfect then

$$f_e(x) = A_1 \exp((-B_1 x^2) + A_2 \exp((-B_2 x^2)). \quad (5)$$

When x=0, then

$$A_2 = f_e(0) - A_1 . (6)$$

In general one of the two exponential terms in equation (5) will decay faster than the other with increasing values of x; if  $A_1 \exp(-B_1x^2) \gg A_2 \exp(-B_2x^2)$  for

large x, and  $x_M$  is the largest value of x for which  $f_e(x)$  is tabulated, we have, to a first approximation,

i.e. 
$$f_e(x_M) = A_1 \exp\left(-B_1 x_M^2\right),$$
$$B_1 = (-1/x_M^2) \ln\left(f_e(x_M)/A_1\right).$$
(7)

Substituting equations (6) and (7) in (5) gives

$$f_e(x) = A_1 \exp \left\{ - (x/x_M)^2 \ln A_1 / f_e(x_M) \right\} + (f_e(0) - A_1) \exp \left\{ -B_2 x^2 \right\}, \quad (8)$$

which contains only two unknown constants,  $A_1$  and  $B_2$ .

Hence for any value of  $A_1$ ,

$$B_{2} = (-1/x^{2}) \times \ln\left\{\frac{f_{e}(x) - A_{1} \exp\left[-(x/x_{M})^{2} \ln\left(A_{1}/f_{e}(x_{M})\right)\right]}{f_{e}(0) - A_{1}}\right\}.$$
 (9)

If the table contains M values of  $f_e(x)$ , equation (9) gives M values for the constant  $B_2$ , with an arithmetic mean  $\overline{B}_2$ , corresponding to the constant  $A_1$ .

Substituting  $\overline{B}_2$  and  $A_1$  in (8), gives the *M* values of e(x). Hence G(x) can be found for each point from equation (2) and  $W_1$ , the sum of the squares of the percentage difference, from (3).

Initially a very small value of  $A_1$  was chosen (0.0001), and this was increased in steps of 0.1 until the condition

$$W_T - W_{(T-1)} > 0 \tag{10}$$

was satisfied, where T denotes the number of cycles, i.e. the number of values of  $A_1$  tried.

When equation (10) is satisfied, the minimum value of W has been passed, and  $A_1$  was changed in steps of -0.01 until equation (14) was again satisfied. The process was repeated, multiplying the increment by -0.1 each time until  $A_1$  had reached a pre-set accuracy. This, together with the corresponding values of  $B_1$ ,  $A_2$ , and  $B_2$ , gives the best fit with the approximations made.

### (b) Second approximation (two terms)

The restrictions given by equations (6) and (7) were relaxed giving four independent variables. Using the method of Vand *et al.* (1957) we have, providing  $\Delta A_j$  and  $\Delta B_j$  are small,

$$\Delta e(x) = \sum_{j=1}^{2} \left( \frac{\partial e(x)}{\partial A_j} \, \Delta A_j + \frac{\partial e(x)}{\partial B_j} \, \Delta B_j \right) \tag{11}$$

and

$$\frac{\partial e(x)}{\partial A_j} = \exp\left(-B_j x^2\right)$$
$$\frac{\partial e(x)}{\partial B_i} = -A_j x^2 \exp\left(-B_j x^2\right). \tag{12}$$

This gives M equations for determining four unknowns  $(\Delta A_1, \Delta B_1, \Delta A_2, \Delta B_2)$ . The equations were solved by the standard least-squares method. Table 1 (columns 3 to 5) gives the results obtained for gold at this stage.

#### (c) Three-term approximation

The three-term expression for  $f_e(x)$  was then used, taking the final values of  $A_1$ ,  $B_1$ ,  $A_2$ ,  $B_2$  from part (b), and setting  $A_3 = B_3 = 0$ . Table 1 shows the results for gold; these are typical of those calculated for other elements.

The values of  $e(x) - f_e(x)$  expressed as a percentage of  $f_e(0)$  are included in Table 1; this criterion was not used in the calculations, but is inserted to illustrate the difference between it and the criterion adopted, which is shown in the preceding column.

Table 1. A comparison of the two-term and three-term approximations to  $f_e(x)$  for gold

		Two terms			Three terms			
			$100[e(x) - f_e(x)]$	$100[e(x) - f_e(x)]$		$100[e(x) - f_e(x)]$	$100[e(x) - f_e(x)]$	
x	$f_{e}(x)$	e(x)	$f_{e}(x)$	$f_{e}(0)$	e(x)	$f_{e}(x)$	$f_{e}(0)$	
0 Å-1	12.90	12.70	-1.51	-1.51	12.90	-0.01	-0.01	
0.05	12.45	12.32	-1.04	-1.01	12.42	-0.22	-0.22	
0.10	11.13	11.26	1.17	1.01	11.16	0.31	0.26	
0.15	9.51	9.77	2.70	1.99	9.53	0.12	0.13	
0.20	7.92	8.14	2.78	1.71	7.92	-0.04	-0.05	
0.25	6.60	6.64	0.57	0.29	6.58	-0.34	-0.18	
0.30	5.58	5.41	-3.03	-1.31	5.55	-0.47	-0.20	
0.35	4.78	4.50	-5.84	-2.16	4.78	0.02	0.01	
0.40	4.14	3.87	-6.58	-2.11	$4 \cdot 17$	0.74	0.24	
0.50	3.19	3.13	-1.89	-0.47	$3 \cdot 22$	1.02	0.25	
0.60	2.53	2.69	6.21	1.22	2.52	-0.44	-0.09	
0.70	$2 \cdot 05$	2.31	12.76	2.03	2.02	-1.61	-0.26	
0.80	1.70	1.95	14.91	1.96	1.67	-1.72	-0.23	
0.90	1.43	1.62	12.95	1.44	1.43	-0.27	-0.03	
1.00	1.22	1.31	7.06	0.62	1.24	1.60	0.12	
1.10	1.05	1.03	-1.64	-0.13	1.08	3.19	0.26	
1.20	0.92	0.80	-13.19	-0.94	0.94	2.66	0.19	
1.30	0.80	0.60	-24.51	-1.52	0.82	$2 \cdot 13$	0.13	
1.40	0.71	0.45	$-37 \cdot 10$	-2.04	0.70	-1.45	-0.08	
1.50	0.64	0.32	-49.54	-2.46	0.59	-7.38	-0.37	
				£ (0)		G D 0 100/ 6	6 (0)	

S.D. = 1.53% of  $f_e(0)$ 

S.D. = 0.19% of  $f_e(0)$ 

# Table 2

(a) Analytic constants for the electron scattering amplitudes (Z=1-18)

				(2 - 1, 10)				
Z	$A_1$	$B_1$	$A_2$	$B_2$	$A_{3}$	$B_3$	Y%	Ref.
1	0.2022	30.8679	0.2437	8.5444	0.0825	1.2726	0.10	$\mathbf{E}$
2	0.052	17.333	0.196	5.686	0.120	0.980	0.09	$\mathbf{H}$
3	1.772	$105 \cdot 507$	1.217	$24 \cdot 456$	0.304	1.863	0.40	$\mathbf{HF}$
4	1.333	$63 \cdot 623$	1.426	16.206	0.323	1.486	0.21	$\mathbf{HF}$
5	1.046	47.281	1.399	11.983	0.356	1.361	0.34	$\mathbf{HF}$
6	0.462	52.702	1.488	11.734	0.463	1.452	0.72	$\mathbf{HF}$
7	0.331	$52 \cdot 839$	1.359	9.817	0.498	1.319	0.32	$\mathbf{HF}$
8	0.303	38.003	1.177	8.193	0.524	1.230	0.23	$\mathbf{HF}$
9	0.206	46.008	1.092	8.334	0.618	1.273	0.22	I
10	0.174	47.002	1.011	7.824	0.659	1.233	0.25	$\mathbf{HF}$
11	2.613	$102 \cdot 813$	1.368	16.207	0.896	1.520	0.38	$\mathbf{HF}$
12	2.578	$62 \cdot 166$	1.599	13.634	0.837	1.313	0.21	$\mathbf{HF}$
13	3.289	41.567	1.431	9.456	0.726	1.070	0.41	I
14	$2 \cdot 447$	$43 \cdot 317$	2.359	$13 \cdot 290$	0.848	1.204	0.32	$\mathbf{H}$
15	1.784	39.795	2.729	12.216	0.855	1.120	0.28	$\mathbf{H}$
16	1.472	36.984	2.756	10.493	0.823	1.050	0.41	$\mathbf{H}$
17	0.728	$55 \cdot 553$	3.103	11.703	1.006	1.235	0.60	I
18	0.268	538.892	3.150	13.345	1.291	1.542	0.55	$\mathbf{HF}$

E: Exact; I: Interpolation; H: Hartree (Hydrogen-like atom method); HF: Hartree Fock.

(b) Analytic constants for the electron scattering amplitudes (Z=20-104). Based on T.F.D. model

(Z = 20-104). Based on T.F.D. model									
Z	$A_1$	$B_1$	$A_2$	$B_2$	$A_{3}$	$B_3$	Y%		
<b>20</b>	2.670	$28 \cdot 184$	1.956	5.739	0.722	0.665	0.36		
<b>21</b>	2.811	$28 \cdot 254$	2.014	5.450	0.719	0.638	0.35		
22	2.872	28.795	2.112	5.576	0.758	0.642	0.19		
<b>23</b>	3.032	$27 \cdot 450$	2.084	5.254	0.766	0.625	0.19		
<b>24</b>	3.033	28.656	2.229	5.536	0.821	0.642	0.16		
<b>25</b>	$3 \cdot 213$	26.504	$2 \cdot 167$	5.109	0.806	0.604	0.15		
<b>26</b>	3.292	27.225	2.264	5.116	0.831	0.602	0.22		
<b>27</b>	3.367	26.715	2.296	5.130	0.866	0.603	0.18		
<b>28</b>	3.382	$27 \cdot 163$	2.399	5.216	0.899	0.607	0.21		
<b>29</b>	3.535	26.480	2.396	4.963	0.900	0.590	0.16		
30	3.558	26.885	2.496	5.063	0.931	0.590	0.18		
31	3.563	$28 \cdot 112$	2.630	5.294	0.987	0.607	0.21		
<b>32</b>	3.693	27.373	2.629	5.176	1.005	0.603	0.18		
33	3.708	27.925	2.716	5.307	1.055	0.612	0.19		
<b>34</b>	3.785	27.657	2.754	5.297	1.086	0.619	0.18		
35	3.822	28.247	2.854	5.290	1.105	0.614	0.16		
36	3.930	27.397	2.841	5.105	1.110	0.596	0.18		
37	4.018	$27 \cdot 126$	2.885	5.032	1.119	0.587	0.18		
38	4.047	27.610	2.963	5.156	1.167	0.597	0.18		
39	4.129	27.548	3.012	5.088	1.179	0.591	0.12		
<b>40</b>	4.102	28.492	3.144	5.277	1.229	0.601	0.12		
41	4.237	27.415	$3 \cdot 105$	5.074	1.234	0.593	0.18		
<b>42</b>	4.294	27.501	3.162	5.103	1.263	0.593	0.18		
<b>43</b>	4.318	28.246	3.270	5.148	1.287	0.590	0.12		
44	4.358	27.881	3.298	5.179	1.323	0.594	0.18		
<b>45</b>	4.431	27.911	3.343	5.153	1.345	0.592	0.17		
<b>46</b>	4.436	28.670	3.454	5.269	1.383	0.595	0.12		
47	4.499	$28 \cdot 259$	3.483	5.196	1.392	0.587	0.19		
48	4.623	27.995	3.482	5.083	1.410	0.586	0.18		
<b>49</b>	4.633	27.983	3.547	5.136	1.441	0.589	0.18		
50	4.628	28.786	3.659	5.258	1.483	0.594	0.18		
51	4.684	28.559	3.679	5.226	1.509	0.593	0.19		
52	4.785	27.999	3.688	5.083	1.500	0.581	0.19		
<b>53</b>	4.761	28.670	3.786	5.273	1.568	0.598	0.12		
54	4.881	28.016	3.767	5.105	1.565	0.584	0.19		
55	4.890	$28 \cdot 839$	3.884	5.207	1.597	0.586	0.19		
56	4.933	28.610	3.907	5.192	1.627	0.589	0.18		
57	4.940	28.716	3.968	5.245	1.663	0.594	0.19		
58	5.007	28.283	3.980	5.183	1.678	0.589	0.18		
59	5.083	28.588	4.043	5.143	1.684	0.581	0.17		
60	5.151	28.304	4.075	5.073	1.683	0.571	0.16		
61	5.201	28.079	4.094	5.081	1.719	0.576	0.17		
<b>62</b>	5.255	28.016	4.113	5.037	1.743	0.577	0.18		

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$\boldsymbol{Z}$	$A_1$	$B_1$	$A_2$	$B_2$	$A_3$	$B_3$	Y%
63	5.286	27.951	4.174	5.026	1.752	0.571	0.19
<b>64</b>	5.225	$29 \cdot 158$	4.314	5.259	1.827	0.586	0.20
65	5.272	29.046	4.347	5.226	1.844	0.585	0.19
66	5.332	28.888	4.370	5.198	1.863	0.581	0.19
<b>67</b>	5.376	28.773	4.403	5.174	1.884	0.582	0.20
68	5.436	28.655	4.437	5.117	1.891	0.577	0.20
69	5.441	$29 \cdot 149$	4.510	5.264	1.956	0.590	0.18
<b>70</b>	5.529	28.927	4.533	5.144	1.945	0.578	0.19
71	5.553	28.907	4.580	5.160	1.969	0.577	0.19
<b>72</b>	5.588	29.001	4.619	5.164	1.997	0.579	0.18
<b>73</b>	5.659	$28 \cdot 807$	4.630	5.114	2.014	0.578	0.18
<b>74</b>	5.709	28.782	4.677	5.084	2.019	0.572	0.19
75	5.695	28.968	4.740	5.156	2.064	0.575	0.19
<b>76</b>	5.750	28.933	4.773	5.139	2.079	0.573	0.17
77	5.754	$29 \cdot 159$	4.851	5.152	2.096	0.570	0.19
<b>78</b>	5.803	29.016	4.870	5.150	2.127	0.572	0.17
<b>79</b>	5.849	29.096	4.906	5.130	2.143	0.571	0.19
80	5.841	29.335	4.973	5.198	2.186	0.577	0.18
81	5.932	29.086	4.972	5.126	2.195	0.572	0.19
82	5.953	28.999	5.016	5.121	2.209	0.568	0.18
83	6.091	$27 \cdot 802$	4.924	4.927	2.193	0.560	0.16
84	6.070	28.075	4.997	4.999	$2 \cdot 232$	0.563	0.17
85	6.133	28.047	5.031	4.957	$2 \cdot 239$	0.558	0.17
86	6.137	28.283	5.105	4.981	2.257	0.556	0.17
87	6.201	28.200	5.121	4.954	2.275	0.556	0.17
88	6.212	28.382	5.170	5.002	2.316	0.562	0.17
89	6.278	28.323	5.195	4.949	2.321	0.557	0.18
90	6.264	28.651	5.263	5.030	2.367	0.563	0.18
91	6.306	28.688	5.303	5.026	2.386	0.561	0.18
92	6.345	28.752	5.347	5.008	$2 \cdot 401$	0.559	0.19
93	6.323	29.142	5.414	5.096	2.453	0.568	0.19
<b>94</b>	6.415	28.836	5.419	5.022	$2 \cdot 449$	0.561	0.19
95	6.378	29.156	5.495	$5 \cdot 102$	2.495	0.565	0.20
96	6.460	28.396	5.469	4.970	2.471	0.554	0.19
<b>97</b>	6.502	28.375	5.478	4.975	2.510	0.561	0.18
98	6.548	28.461	5.526	4.965	2.520	0.557	0.19
99	6.526	$28 \cdot 806$	5.605	5.038	2.560	0.559	0.18
100	6.559	28.924	5.644	5.044	2.586	0.561	0.19
101	6.570	29.214	5.708	5.070	2.612	0.562	0.19
102	6.619	29.184	5.730	5.055	2.632	0.561	0.21
103	6.598	29.686	5.817	5.142	2.674	0.566	0.20
104	6.627	$29 \cdot 815$	5.860	5.161	2.701	0.567	0.21

With three terms, it can be seen that each point is fitted with an error of less than 2% of  $f_e(x)$  up to  $\sin \theta/\lambda = 1.0$  Å<sup>-1</sup>. This is typical for all elements with Z > 20, but for Z = 1-18 this accuracy of fit only extends out to 0.6 Å<sup>-1</sup> in general. For points where the error is larger than 2% the differences are still regarded as being sufficiently small to be ignored for most practical purposes.

#### Results

The values of the parameters calculated for all elements (excluding Z=19) are listed in Table 2, where the last column gives the standard deviation of the analytical curve expressed as a percentage of  $f_e(0)$ ; the average value of the standard deviation is 0.22%. These values are for electrons of mass  $m_0$ .

The relativistic correction is obtained by multiplying the three A parameters by

$$\left[1-\frac{v^2}{c^2}\right]^{-\frac{1}{2}},$$

where v is the electron velocity and c is the velocity of light.

It is interesting to compare the values of the parameters obtained for different elements. For light atoms (Z < 20) the shell structure affects the value of  $f_e(x)$  greatly, and hence there are larger fluctuations in the parameters. However, for elements with Z > 20, where the T.F.D. model of the atom was used to obtain f(x) and hence  $f_e(x)$  the A values were found to increase fairly smoothly with increasing Z, and the values of  $A_3$ , for example, lie within 4% of the line

$$\log_{10} (A_3) = 0.82 [\log_{10} (Z) - 1.5].$$

Similar equations were obtained for  $A_1$  and  $A_2$ . The *B* parameters did not exhibit any such smooth variation with *Z*.

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# The Crystal Structure of $K_3SiF_7$

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A fine-grained homogeneous powder of composition  $K_3SiF_7$  results from dry ignition of  $K_2SiF_6$  to about 700 °C. Analysis of the powder data establishes that  $K_3SiF_7$  is tetragonal with a = 7.740, c = 5.564 Å. A calculated powder diffraction diagram for a structure in  $P4/mbm-D_{4h}^5$  agrees with the observed diagram with average departures less than 30%. The structure is a tetragonal honeycomb of composition  $K_2SiF_6$  which adducts strings of alternating K and F ions.

A previous investigation by one of us (Deadmore, 1960) of the thermal stability of  $K_2SiF_6$  in dry air revealed that at temperatures of 700 to 750 °C. it loses  $SiF_4$  until the composition  $K_3SiF_7$  is reached.

The K<sub>3</sub>SiF<sub>7</sub> used here was prepared by heating K<sub>2</sub>SiF<sub>6</sub> in dry air for 2 hr. at 750 °C. A chemical analysis gave 41.4% K, 10.2% Si, and 47.4% F, which agrees well with the calculated composition of 42.0% K, 10.2% Si, and 47.8% F. The measured density was 2.86 g.cm.<sup>-3</sup>, and the calculated density, using the cell constants given below and Z=2, is 2.78 g.cm.<sup>-3</sup>.

The product is fine-grained, and affords only a powder diffraction diagram, but inspection of the data suggests isomorphism with the  $(NH_4)_3SiF_7$  crystal analyzed by Hoard & Williams (1942). Powder lines were all found to be indexable on the basis of a tetragonal cell with a = 7.740 and c = 5.564 Å (both  $\pm$  about 1/20 of 1%), with a/c = 1.391, and a trial structure in  $P4/mbm-D_{4\hbar}^5$  afforded reasonable interatomic distances. The crystallization has a large temperature amplitude, and complete  $\alpha_1 - \alpha_2$  resolution is not realized within the range of unambiguous indexing. The accuracy estimate for lattice parameters is based on the absence of significant drift in calculated values between 50° and 70° 2 $\theta$  with Cu radiation.

The disadvantage of being confined to powder data was in part offset by the advantage that the scattering power of potassium substantially exceeds that of the other constituents, with the result that some large index lines were probably properly indexed to d values as small as 0.889 Å.

Table 1. Atom parameters for K<sub>3</sub>SiF<sub>7</sub> in P4/mbm\*

- $2 K_{I}$  in 2(a) 0, 0, 0;  $\frac{1}{2}$ ,  $\frac{1}{2}$ , 0

 $8 F_{III}$  in 8(k) x,  $x + \frac{1}{2}$ , z, etc. with x = 0.390 and z = 0.216

\* Correspondence with the Hoard & Williams analysis is effected by the substitution x = -x.

Variable parameters are most sensitive to intensities of the reflections for which h+k is odd. Fourteen of these were observed, resolved from neighboring features, among reflections up to  $\sin \theta / \lambda = 0.5$ , and five more fell at positions where lines could have been observed if present. The parameters selected in Table 1 are those affording apparent best agreement under an assumption that the six  $SiF_6$  octahedral distances were equal. After application of an arbitrary temperature factor, they give average departures of  $|I_o - I_c|/I_o$  of 0.28 (comparable with a reliability factor of about 0.15) for the 14 observations, and calculated intensities for the 5 possibilities not found or doubtful, were all trivial. Eight other h+k odd reflections fell in mutual doublets, for which intensity sums show adequate agreement.